



# Integration of DIC into VFM: how do measurements contribute to identified material properties?

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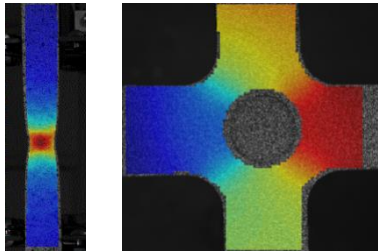
\* University of Southampton

Celebrating 50 years of BSSM:  
Showcase on leading edge experimental techniques,  
4th November 2014 , London UK



# Motivation

## Full-Field measurements



- Grid
- Photoelasticity
- Interferometry
- Digital Image Correlation
- ...

**Measurement errors**



## Mechanical properties of materials

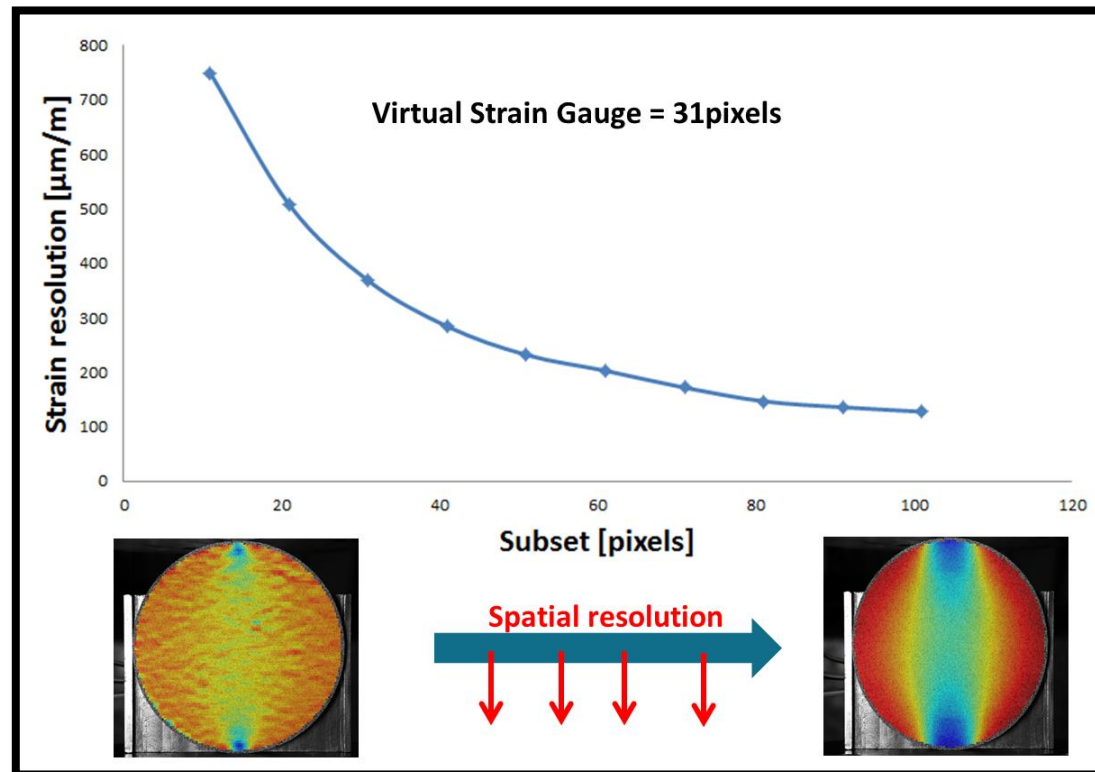
- Finite element updating
- Constitutive equation gap
- Equilibrium gap
- Reciprocity gap
- Virtual Fields Method
- ...

**Identification errors**

# DIC is a complex and non-linear process

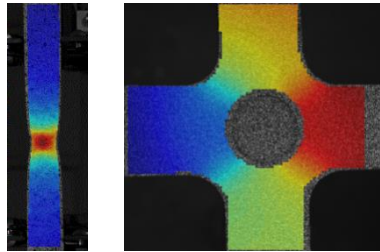
... results depend on many parameters:

- Correlation criterion
- Interpolation routines
- Shape functions
- Regularization parameters:
  - Subset
  - Virtual strain gauge size
- Speckle pattern
- ...



# Motivation

## Full-Field measurements



- Grid
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- ...

**Measurement errors**

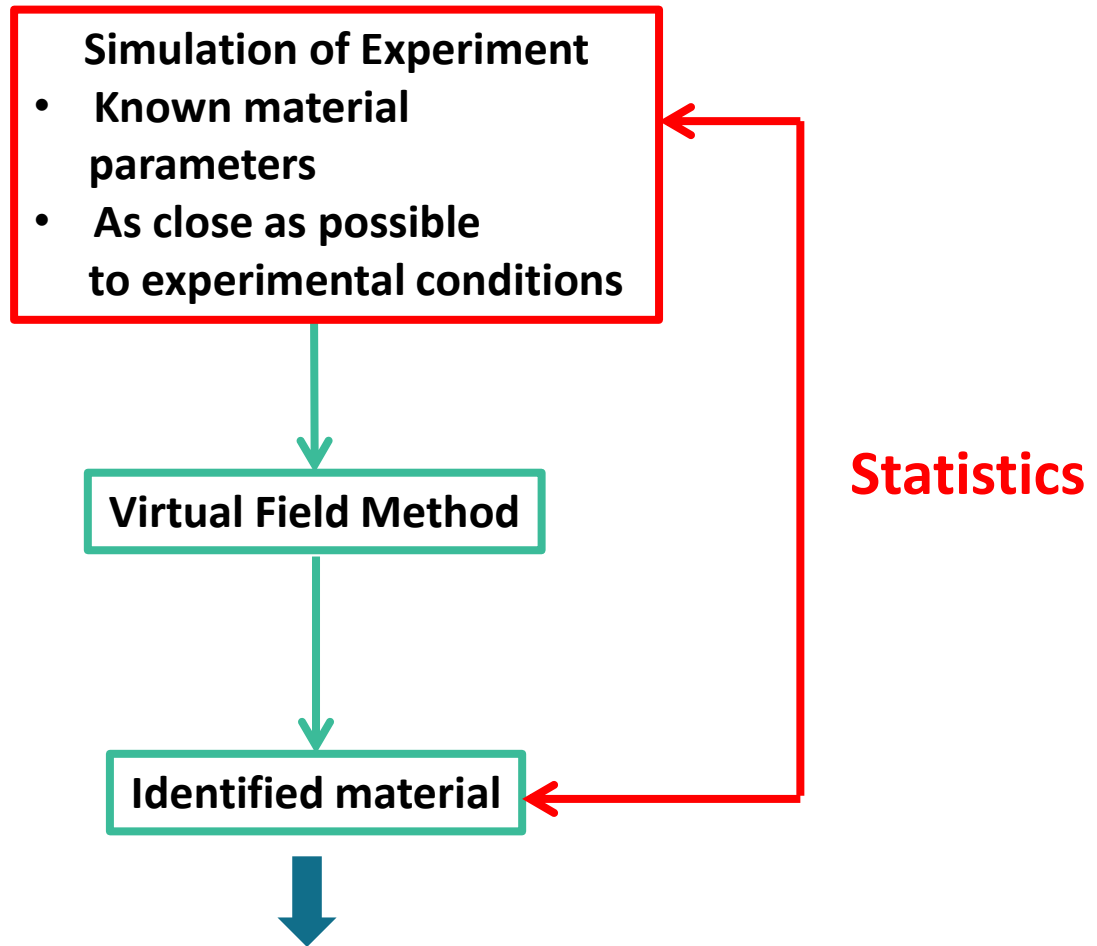
## Mechanical properties of materials

- Finite element updating
- Constitutive equation gap
- Equilibrium gap
- Reciprocity gap
- Virtual Fields Method
- ...

**Identification errors**

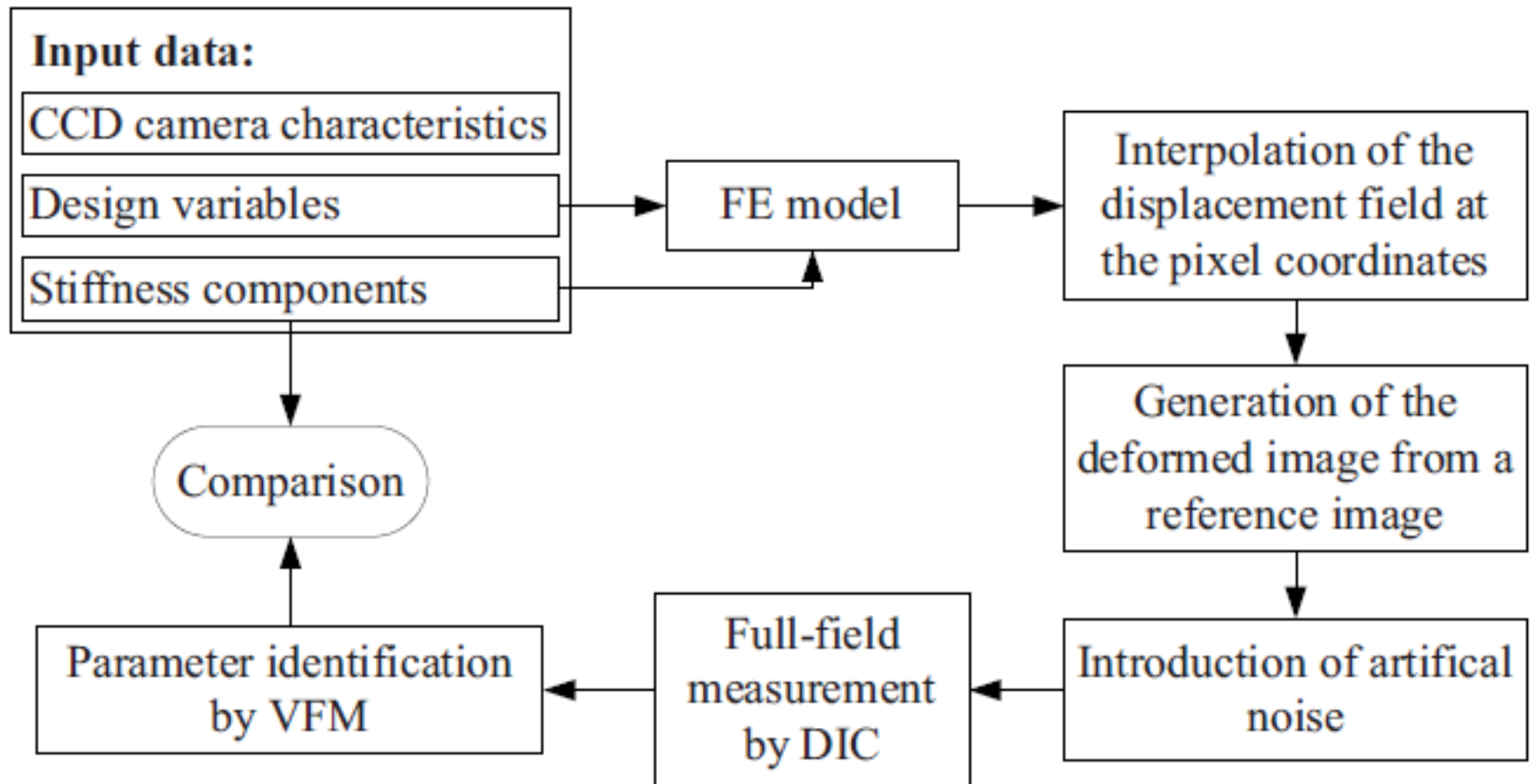
**Any realistic UQ on the mechanical parameters requires to take into account the measurement process**

# How?

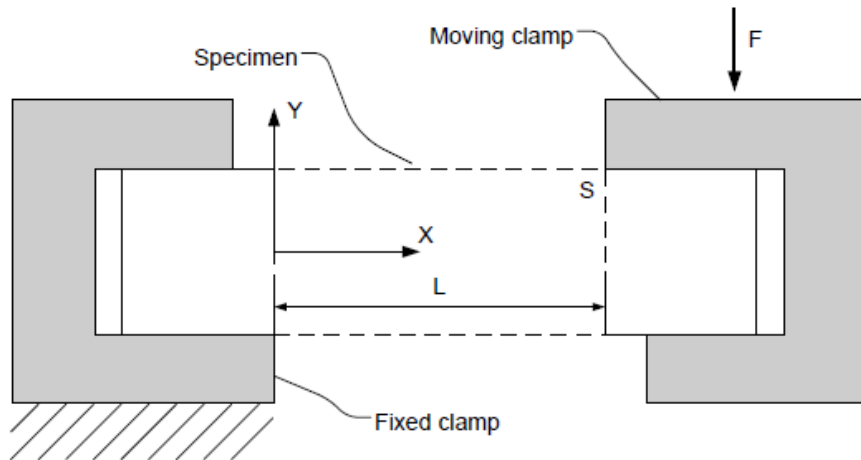


- **Confidence margins** for the determined material parameters
- **Optimization** of test design (geometry of specimen, smoothing , ... )

# Simulate the whole identification chain



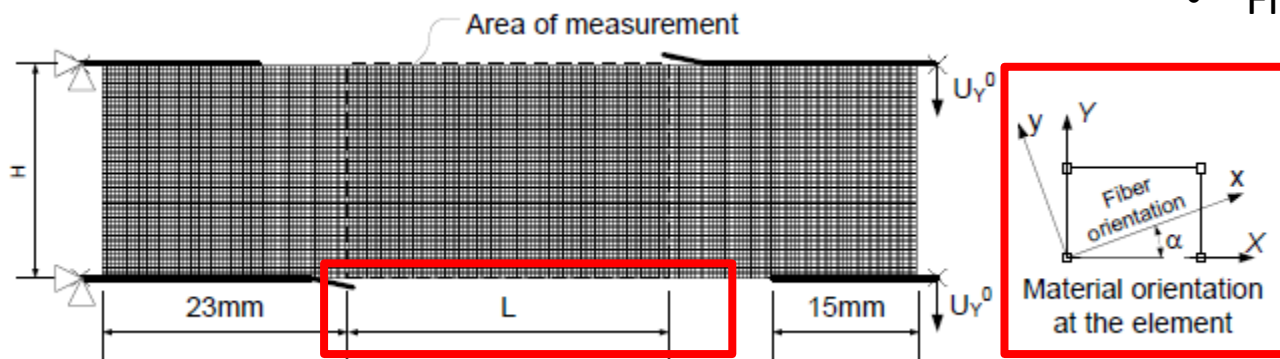
# Case study : unnotched Iosipescu test



- Glass/epoxy unidirectional composite
- Linear elastic orthotropic

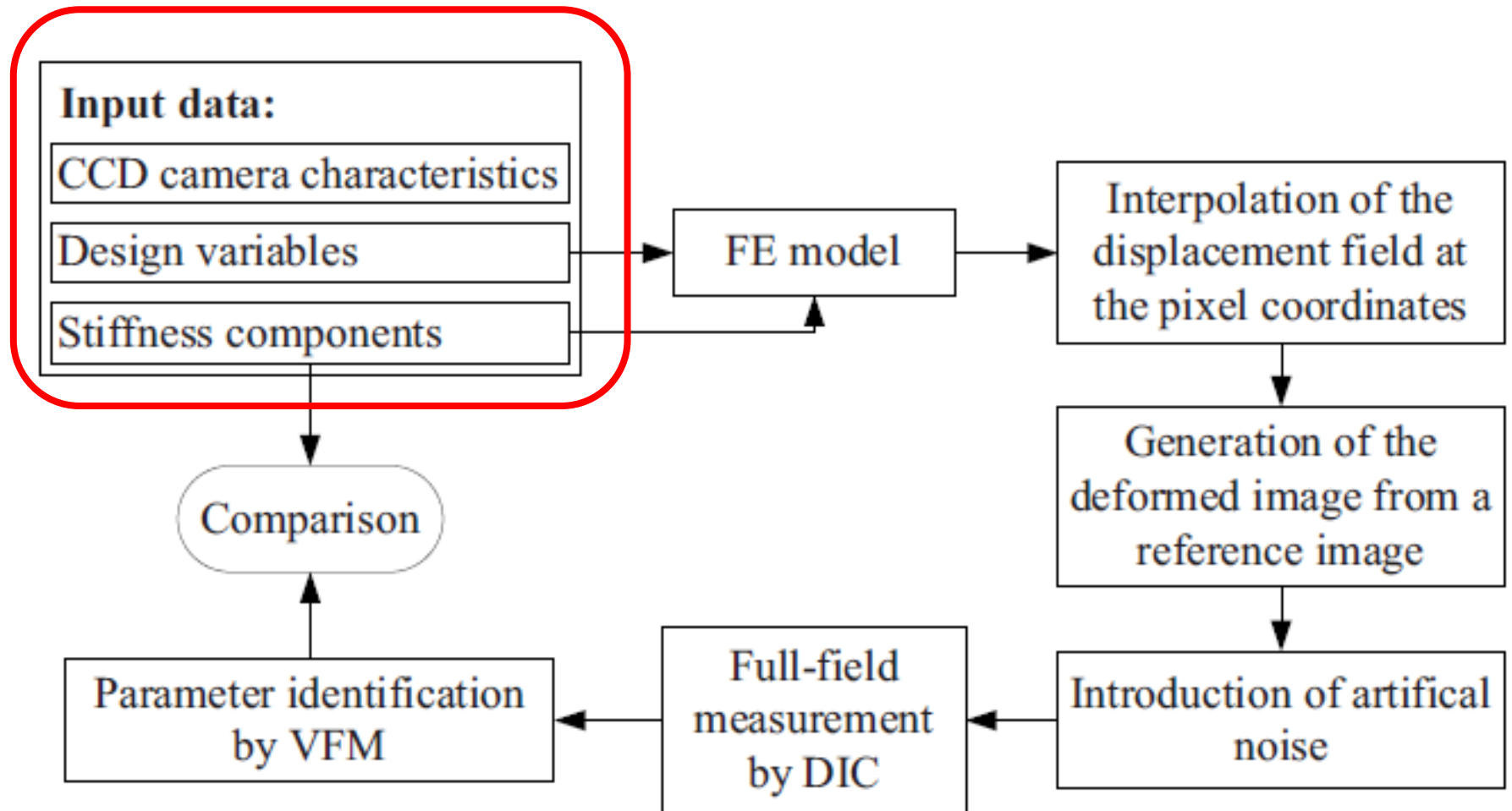
Stress state is composition of compression, bending and shear

- **Design variables:**
  - Free length  $L$
  - Fibre orientation  $\alpha$



Rossi M., Pierron F., International Journal of Solids and Structures, 2012.

# Simulate the whole identification chain





# Input data

## Design Variables

- Free Length L:  
10 -> 60 mm ; L = 2mm
- Fibre orientation  $\alpha$ :  
 $0^\circ$  ->  $90^\circ$  ;  $\alpha$  +=  $10^\circ$

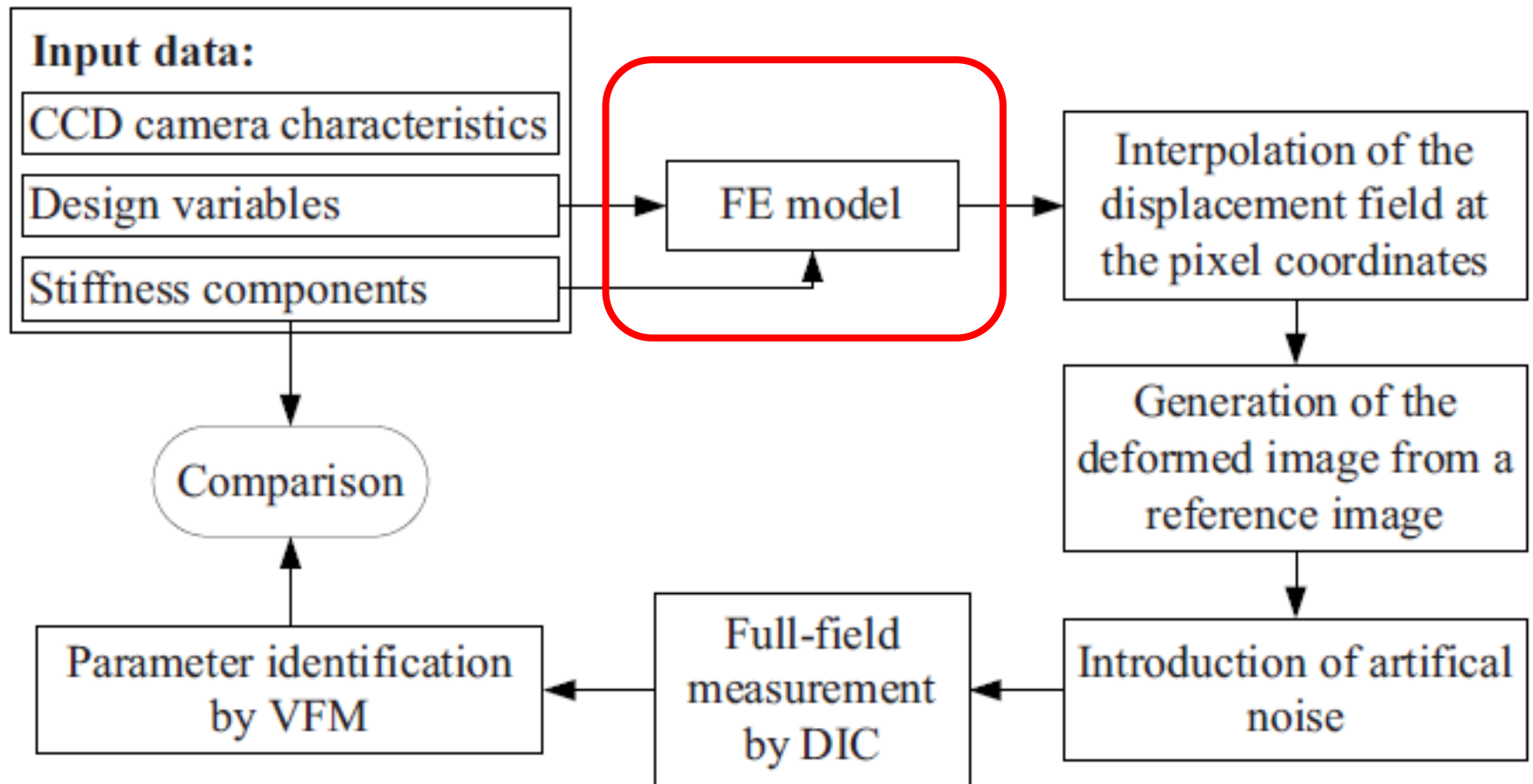
## Camera characteristics

- spatial resolution: 1320 x 1024
- Dynamic range: 8-bit

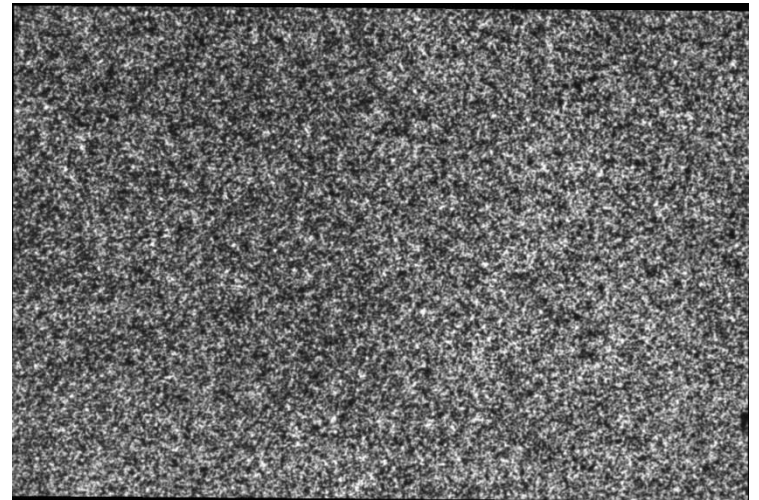
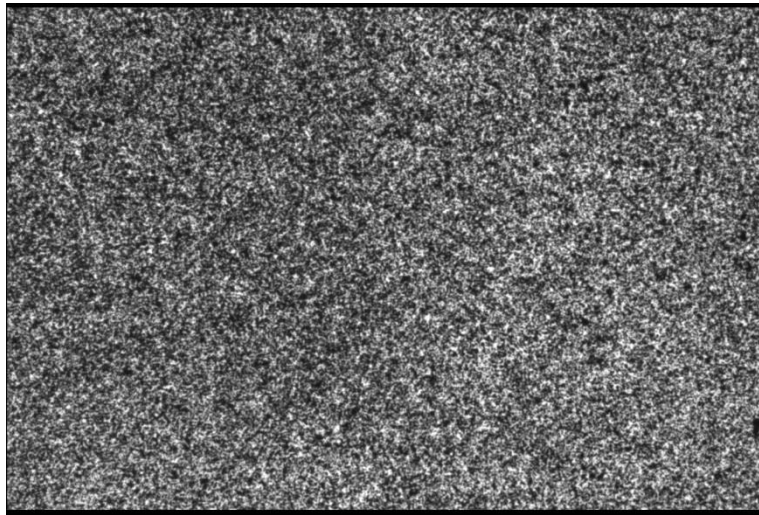
## Stiffness components

Stiffness		Maximum stress	
$Q_{xx}$ (MPa)	40920	$S_{+x}$ (MPa)	1000
$Q_{yy}$ (MPa)	10230	$S_{-x}$ (MPa)	-600
$Q_{xy}$ (MPa)	3069	$S_{+y}$ (MPa)	40
$Q_{ss}$ (MPa)	4000	$S_{-y}$ (MPa)	-100
		$S_s$ (MPa)	40

# Simulate the whole identification chain

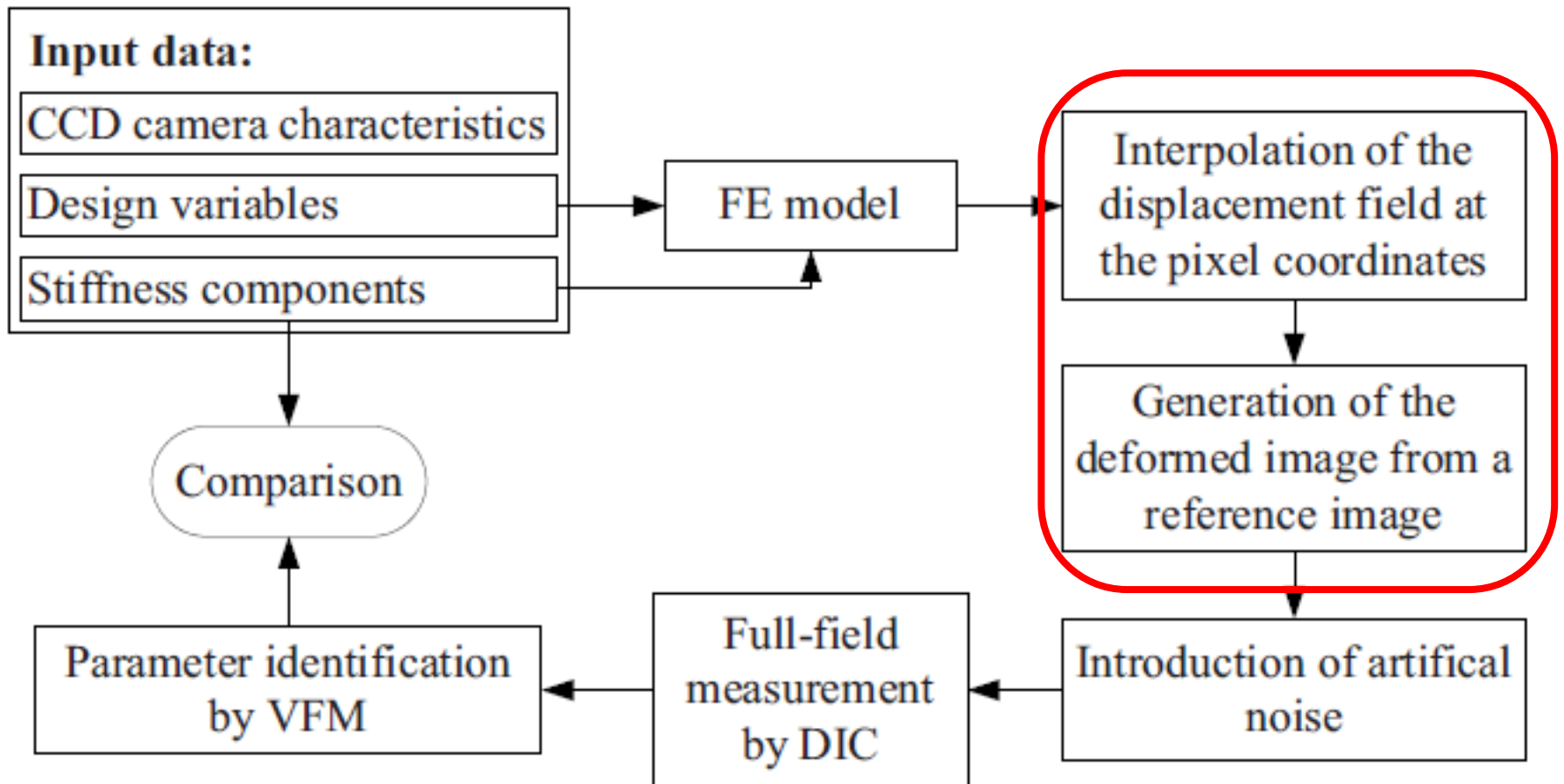


# FE generated displacement map + image of real speckle pattern



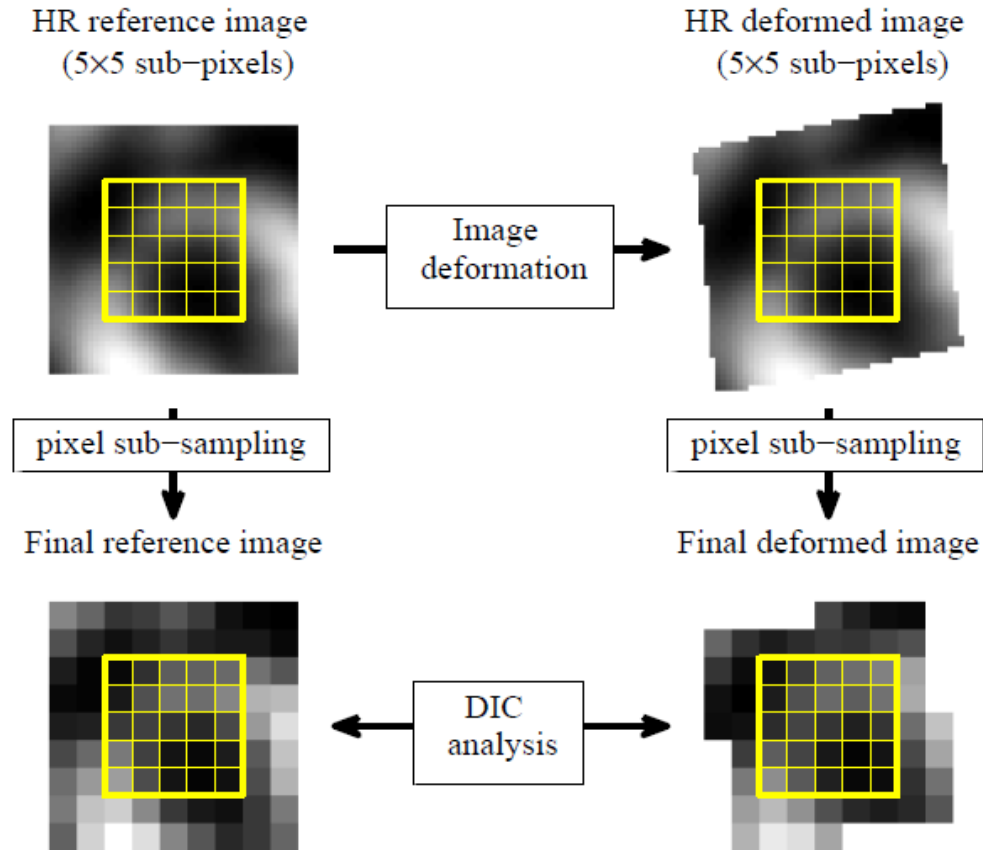
**SPECKLE DEFORMATION**

# Simulate the whole identification chain

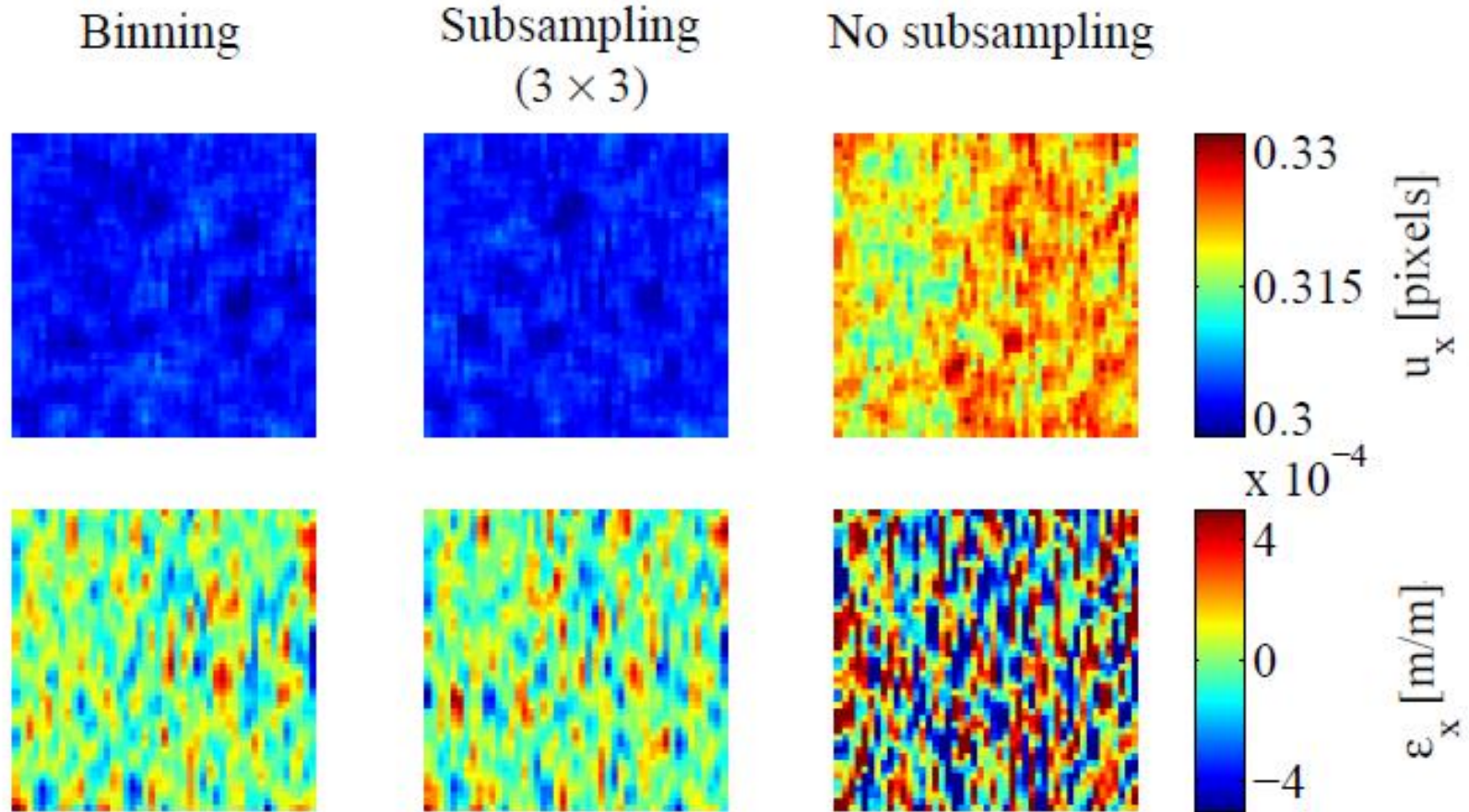


# Synthetic image generation

Numerical deformation errors should be as low as possible: SUB-SAMPLING



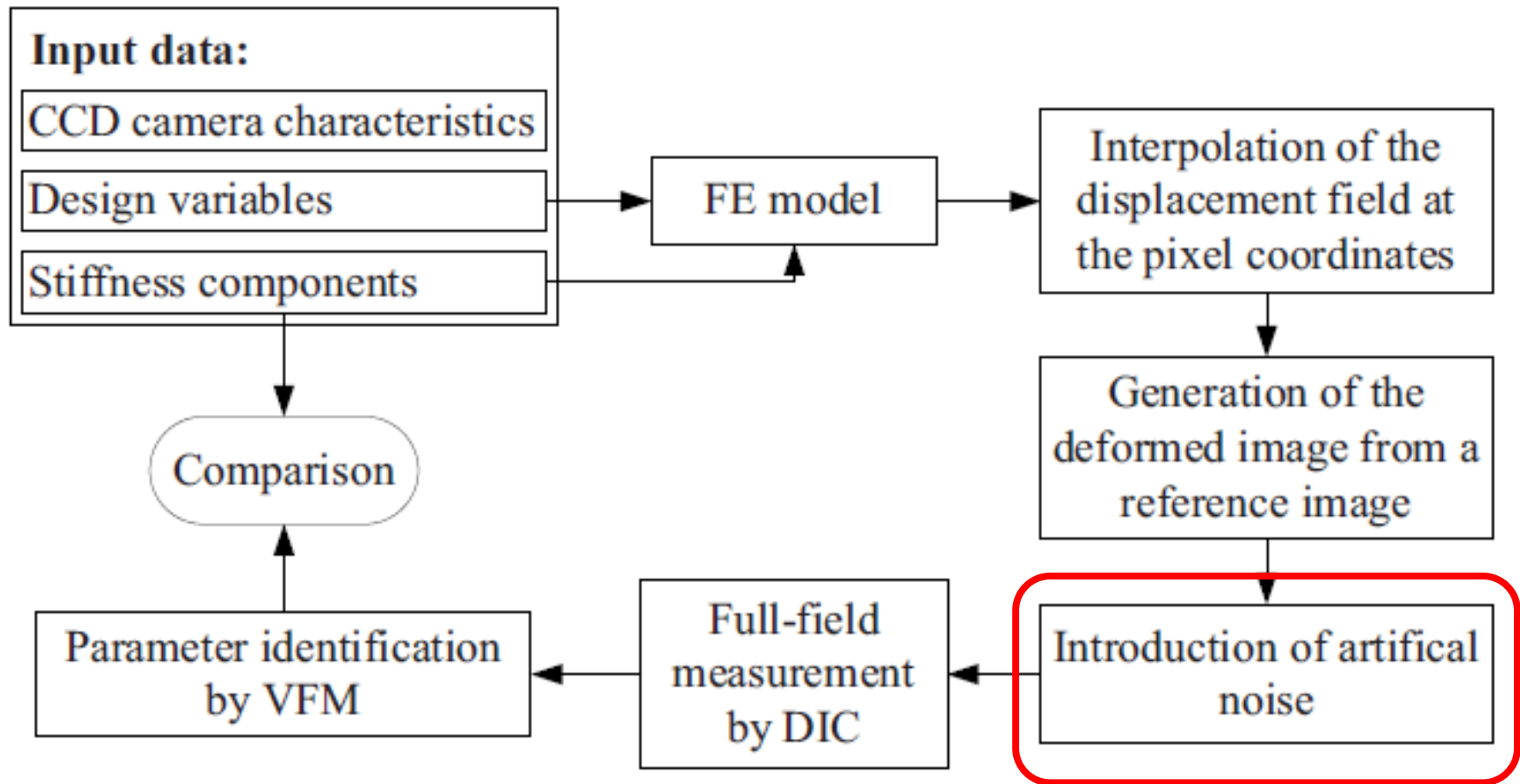
# Synthetic image generation: validation



P. Reu, *Experimental and numerical methods for exact subpixel shifting*,  
Experimental Mechanics 51 (2011) 443-452

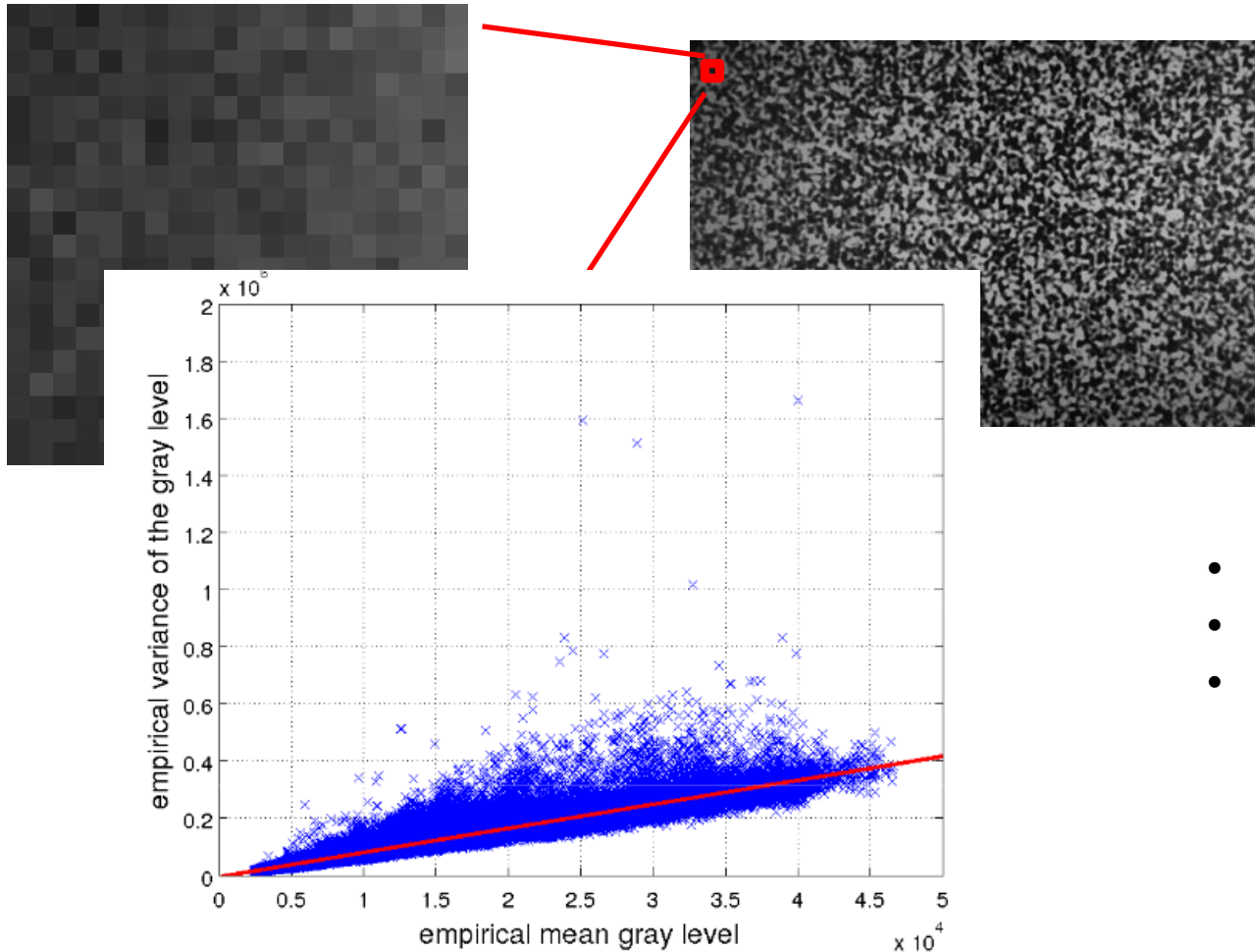
Rossi M., Lava P., Pierron F., Debruyne D. and Sasso M. *Effect of DIC spatial resolution, noise and interpolation error on identification results with the VFM*, submitted to Strain (2014)

# Simulate the whole identification chain



# Noise ...

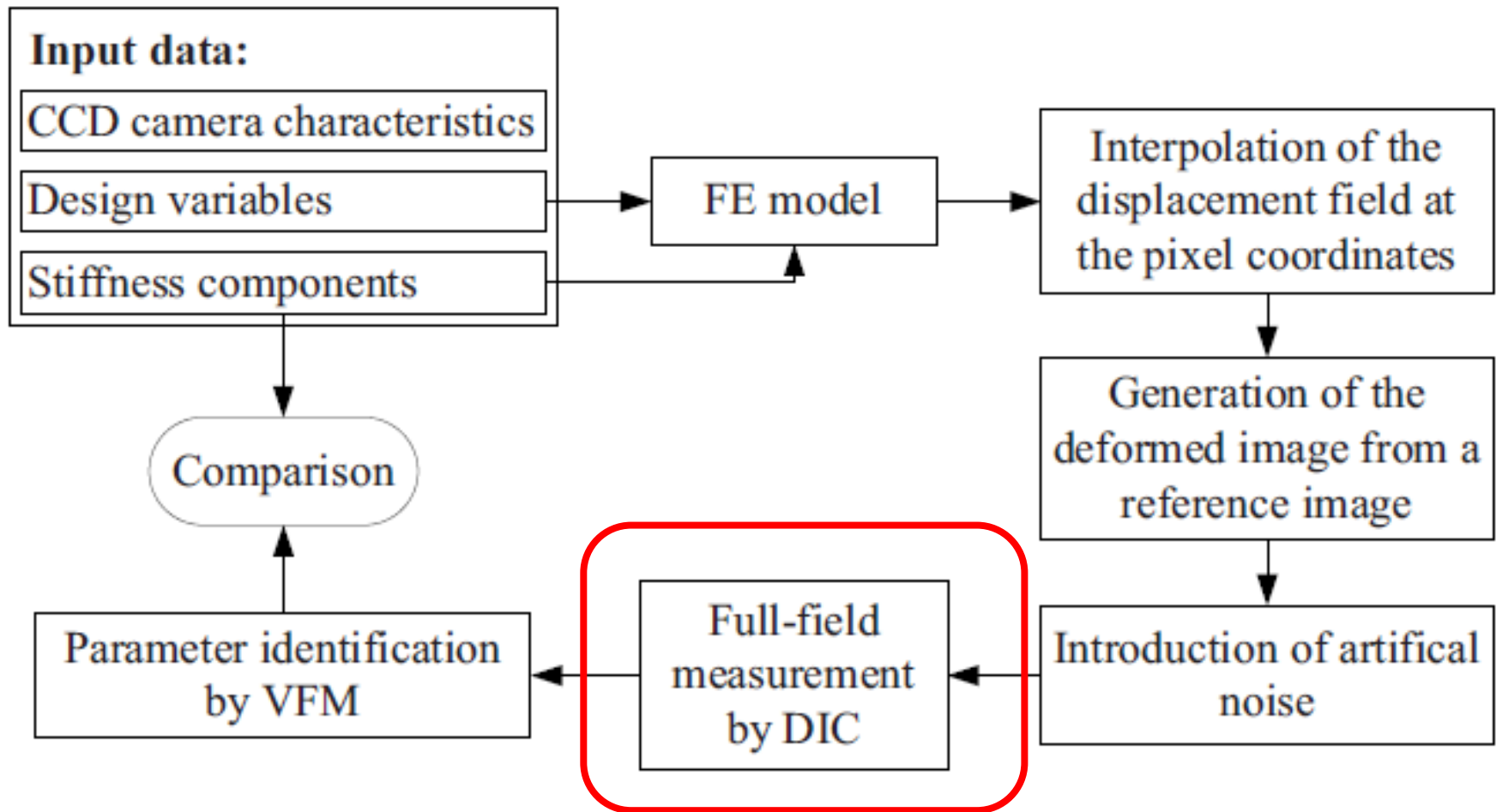
Intensity/color fluctuation around the “actual” image intensity/color.



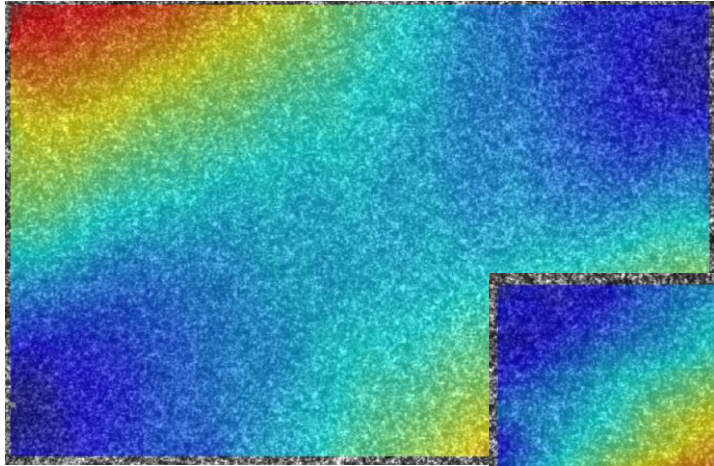
- Gaussian
- Poisson-Gaussian
- Extreme Value



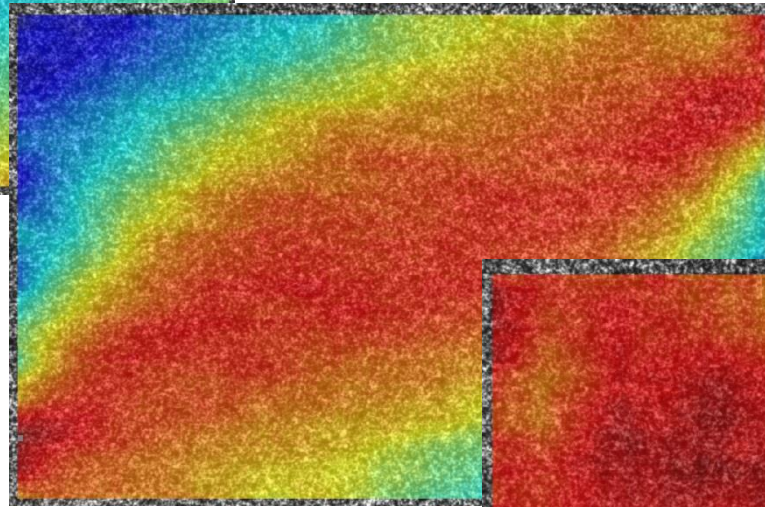
# Simulate the whole identification chain



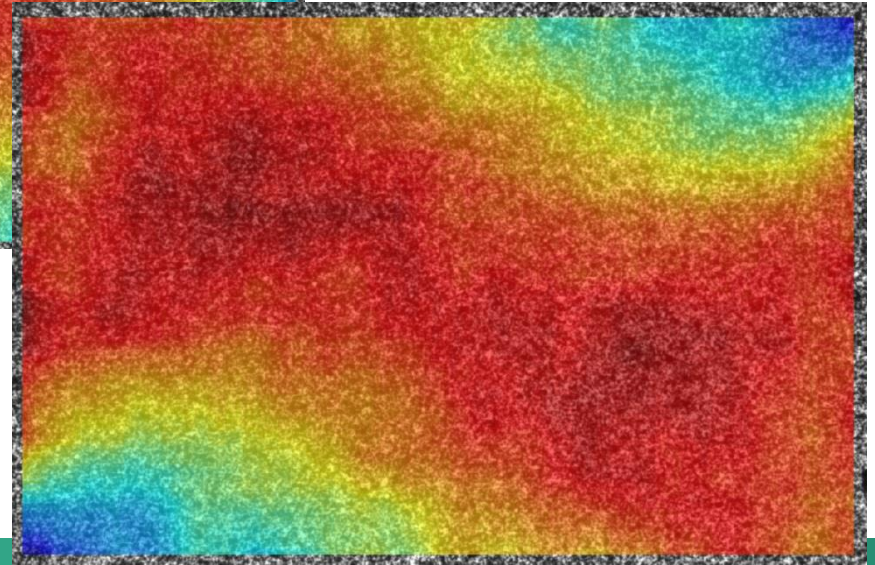
# Full-field measurement by DIC



$E_{xx}$

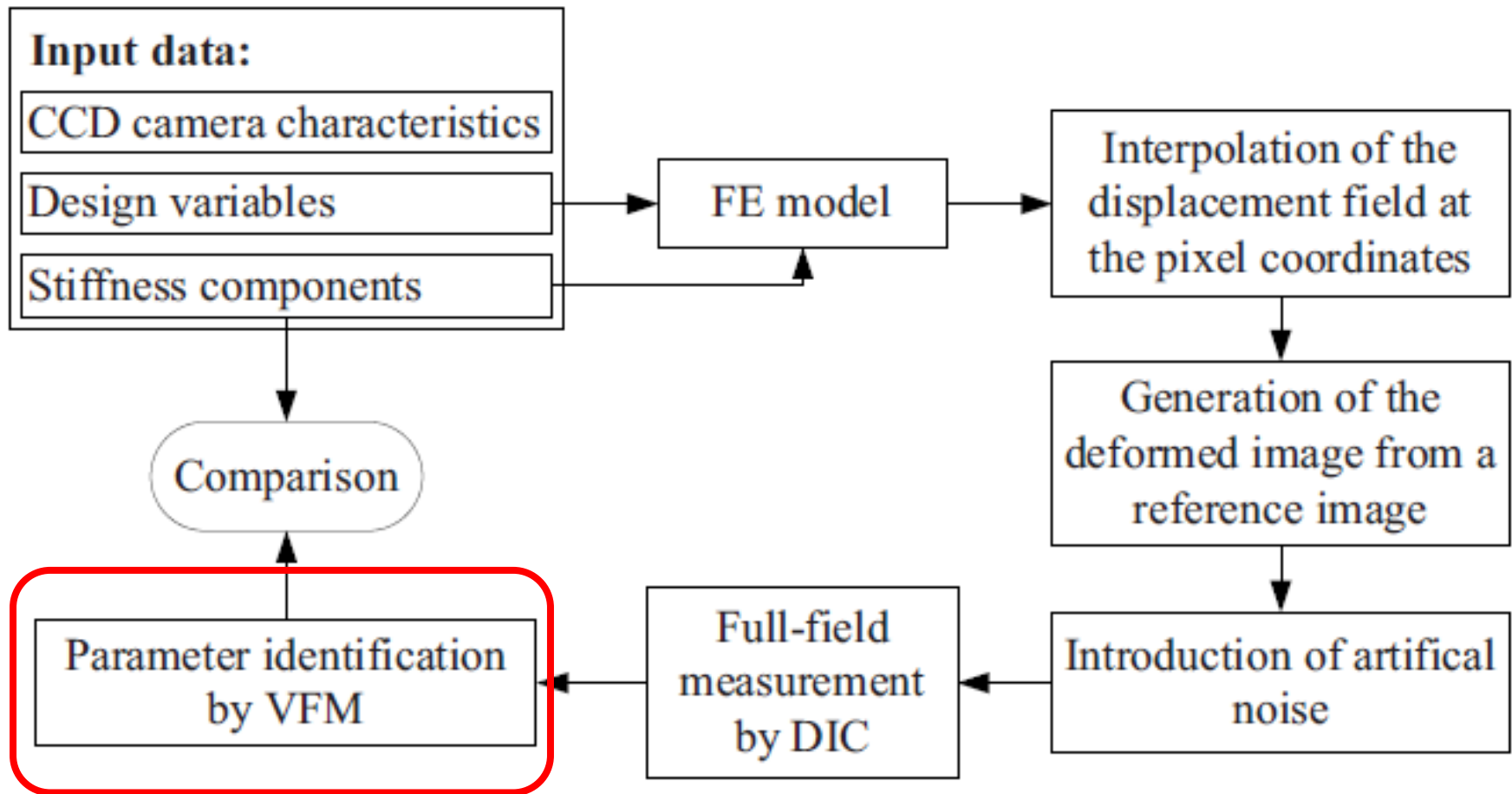


$E_{yy}$

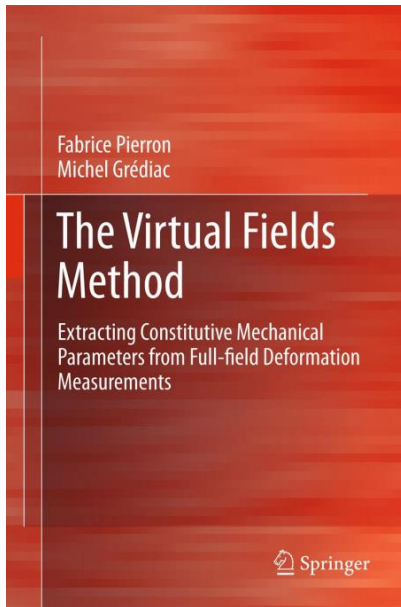


$E_{xy}$

# Simulate the whole identification chain



# Virtual Fields Method



Based on the principle of virtual work:

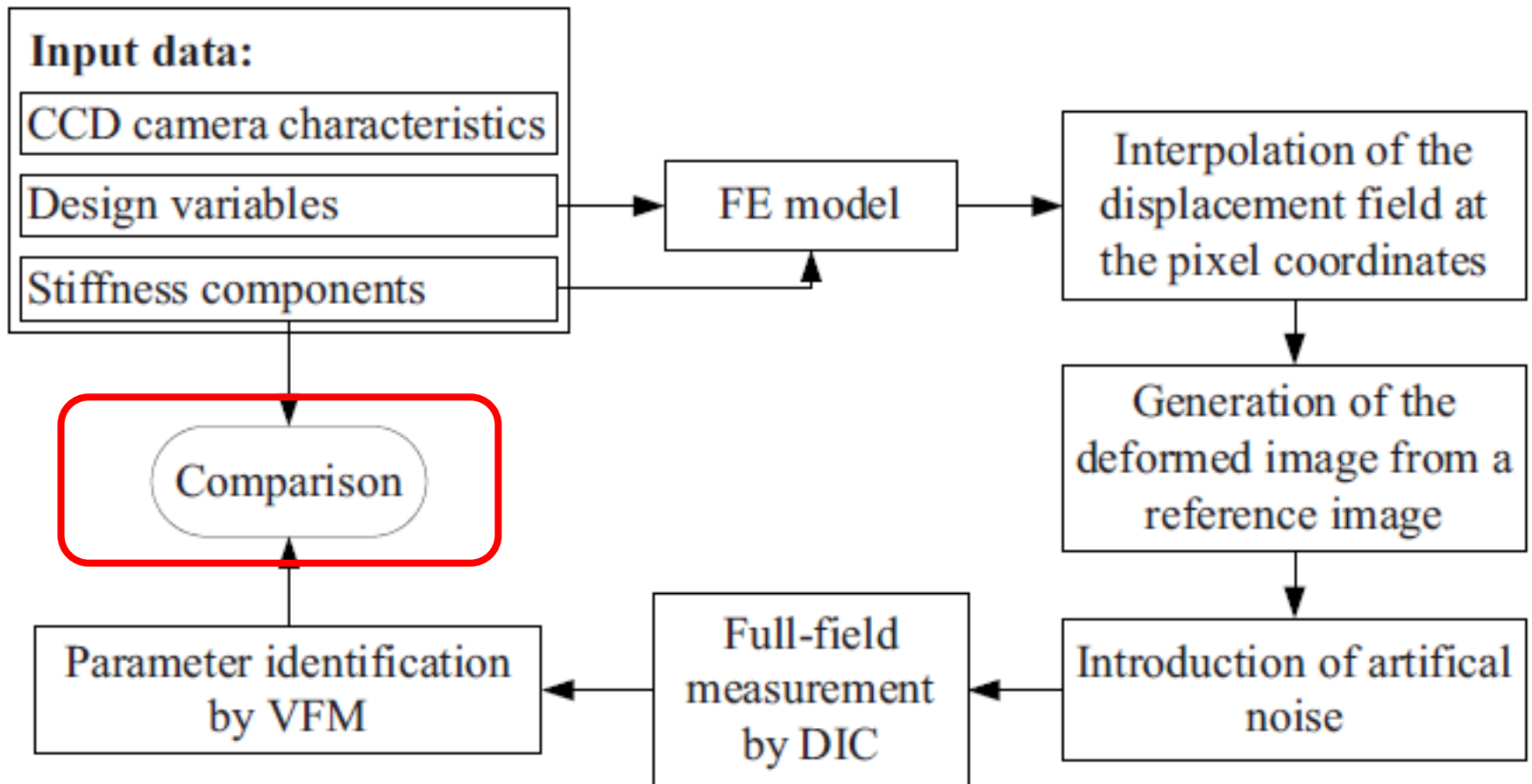
$$\underbrace{- \int_V \sigma : \epsilon^* dV}_{W^*_{int}} + \underbrace{\int_S \bar{\mathbf{T}} \cdot \mathbf{u}^* dS + \int_V \mathbf{b} \cdot \mathbf{u}^* dV}_{W^*_{ext}} = \underbrace{\int_V \rho \mathbf{a} \cdot \mathbf{u}^* dV}_{W^*_{acc}} \quad \forall \mathbf{u}^* \in \text{KA}$$



Homogeneous linear elastic orthotropic materials

$$\begin{aligned}
 Q_{xx} \int_S \epsilon_x \epsilon_x^* dS + Q_{yy} \int_S \epsilon_y \epsilon_y^* dS + Q_{xy} \int_S (\epsilon_x \epsilon_y^* + \epsilon_y \epsilon_x^*) dS + \\
 Q_{ss} \int_S \epsilon_s \epsilon_s^* dS = \int_{\partial S} T_x u_x^* dl + \int_{\partial S} T_y u_y^* dl
 \end{aligned}$$

# Simulate the whole identification chain



# comparison

The **identification error** is defined as

$$Err = \sqrt{\sum_{ij} w_{ij} \left(1 - \frac{Q_{ij}}{Q_{ij}^0}\right)^2}$$

with  $ij = [xx, yy, xy, ss]$

$Q_{ij}^0$  are the reference parameters introduced in the FE model

$Q_{ij}$  are the parameters identified with the VFM

$w_{ij}$  is a weighting parameter

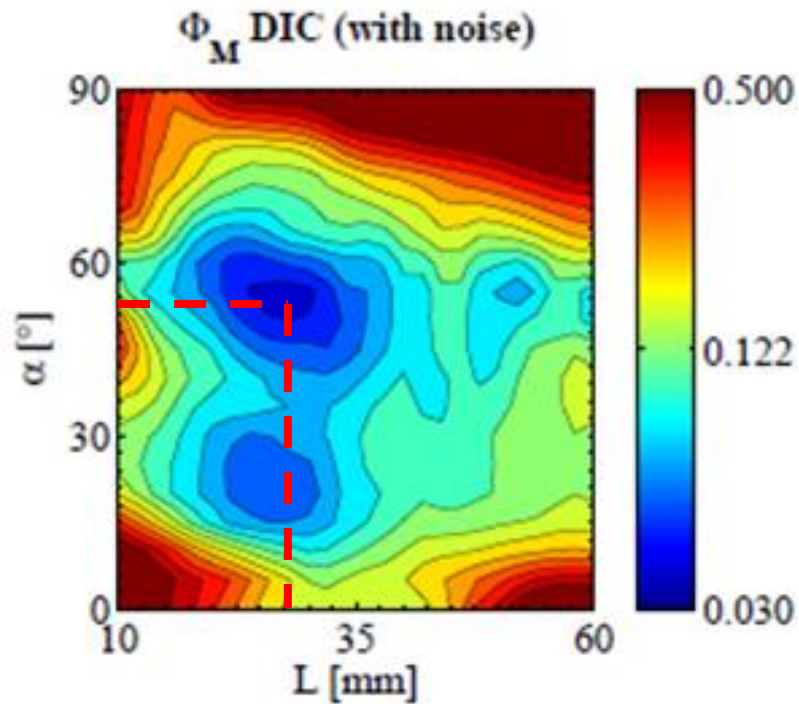
Noise introduction (random): **several** simulated experiments are repeated

$$Err = \frac{1}{N_e} \sum_{k=1}^{N_e} Err_k$$

# Optimization in view of TEST DESIGN

SS = 21 , VSG = 201 are FIXED

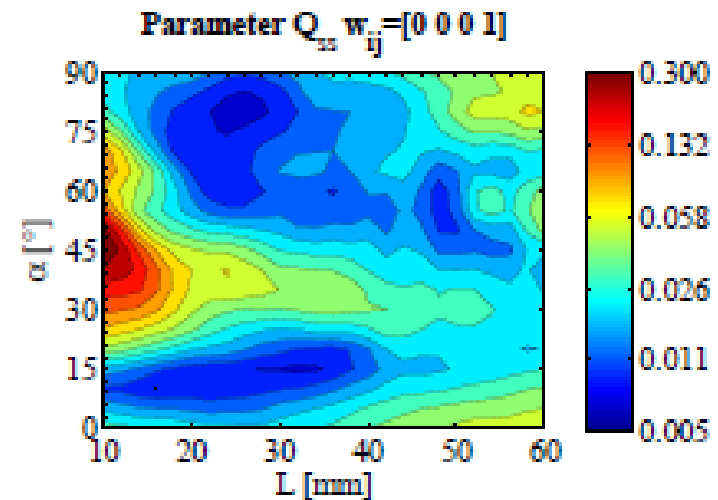
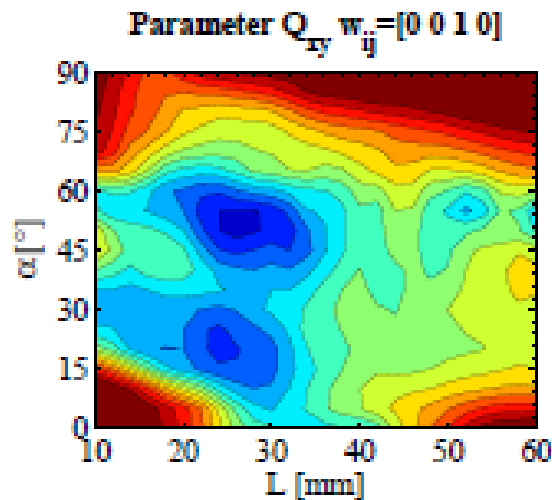
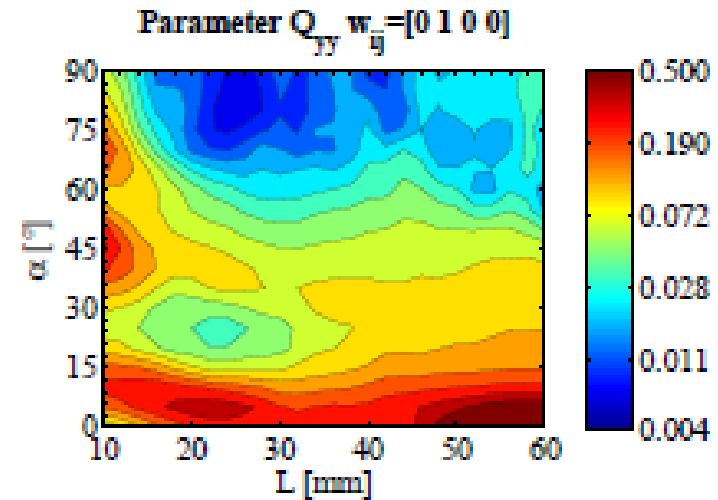
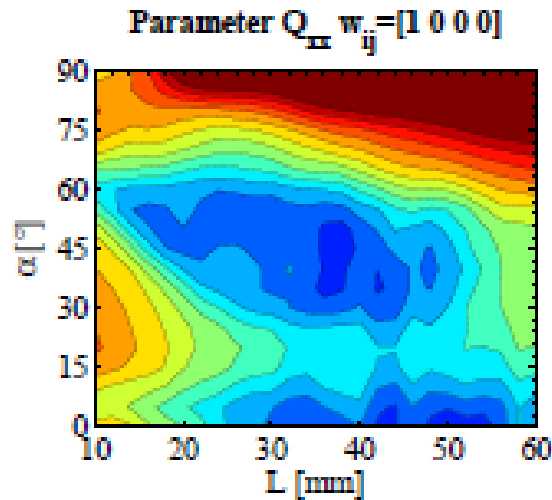
(1360x1024 ; noise: 2 grey levels; 8-bit; 20 repetitions;  $\Delta L = 2\text{mm}$  ;  $\Delta\alpha = 10^\circ$ )



Optimum  $L = 30$  mm and  $\alpha = 50-60^\circ$

Rossi M., Lava P., Pierron F., Debruyne D. and Sasso M. *Effect of DIC spatial resolution, noise and interpolation error on identification results with the VFM*, submitted to Strain (2014)

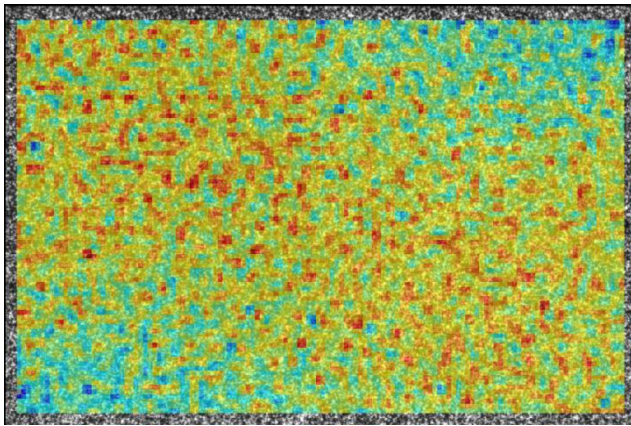
# Results



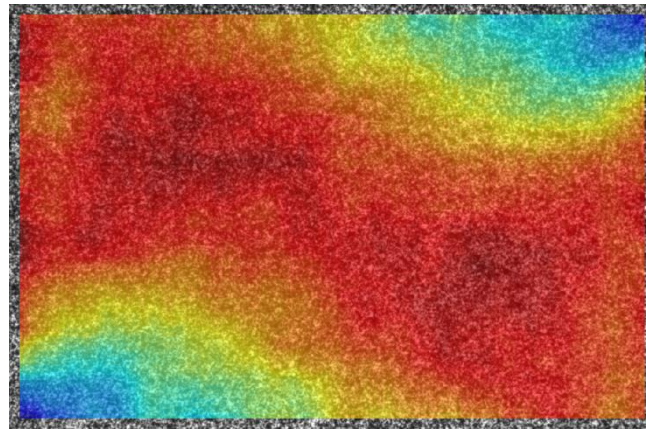


# Optimization in view of Regularization

- Shear strain maps obtained by image deformation plus different levels of smoothing



VSG=5 pixels  
(no smoothing)

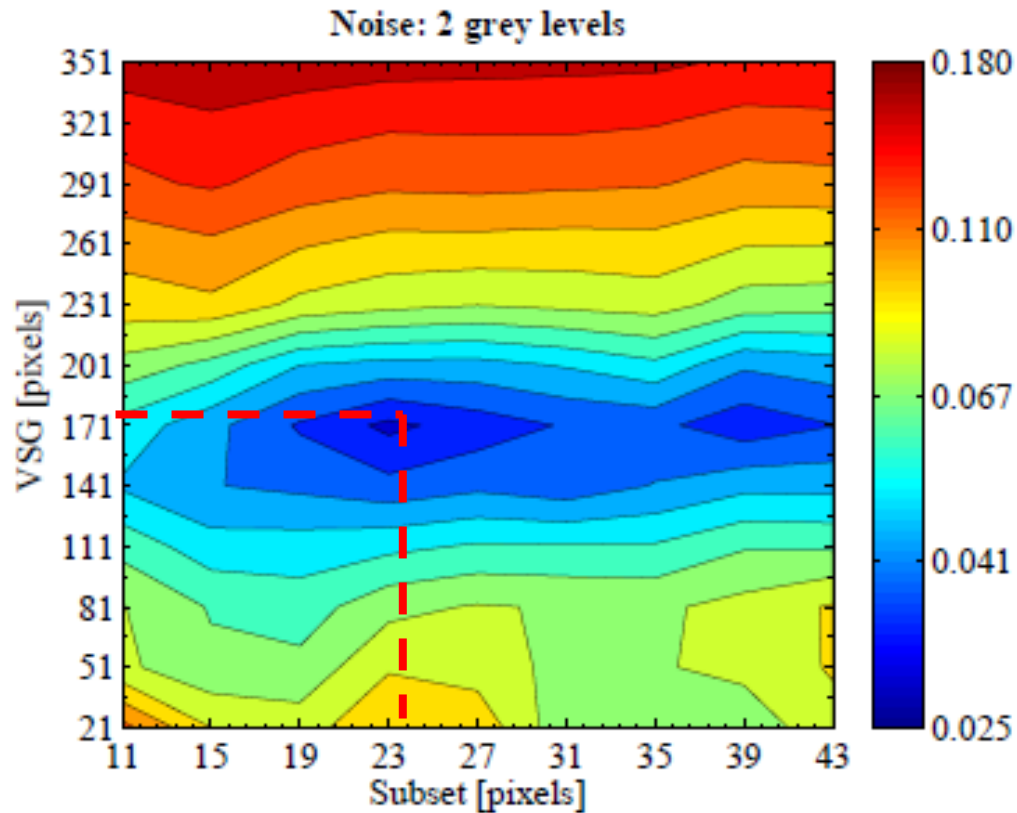


VSG=60 pixels  
(local polynomial)

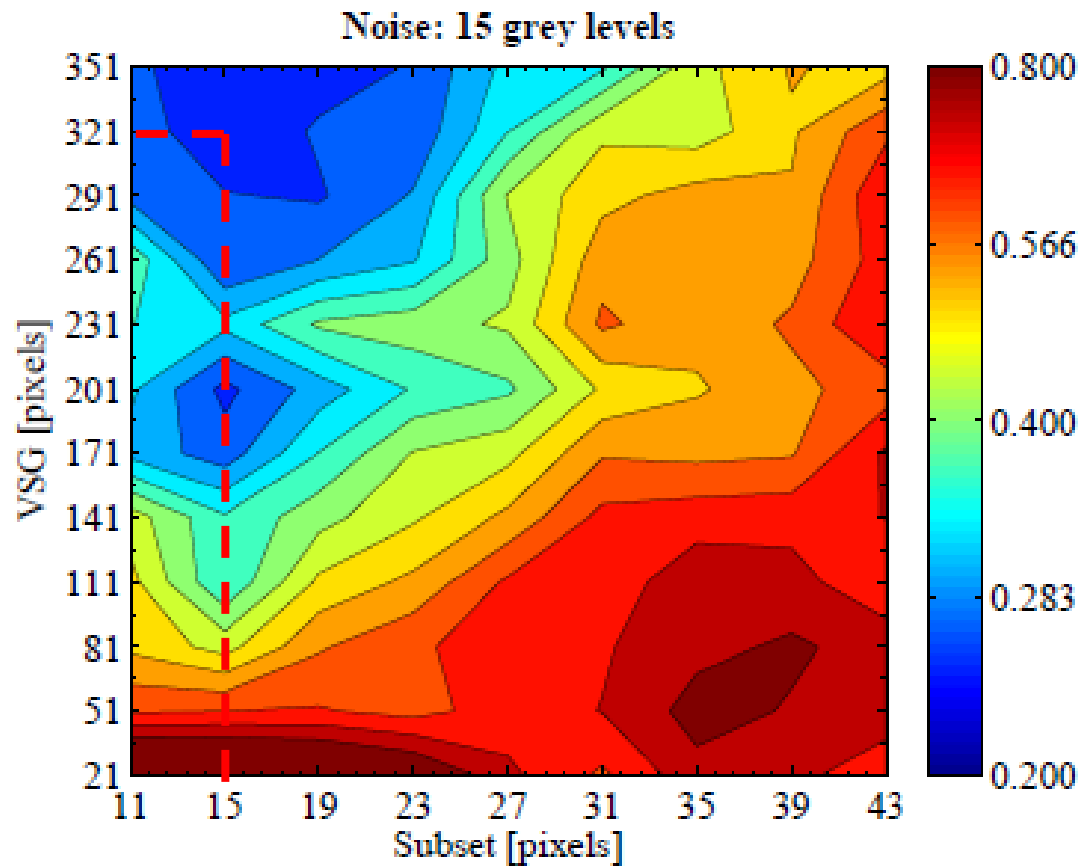
Which one is 'the best' ?

# Results

$L = 30 \text{ mm}$ ,  $\alpha = 55^\circ$  are FIXED: optimization in view of **DATA ANALYSIS**



Smoothing ... but not too much

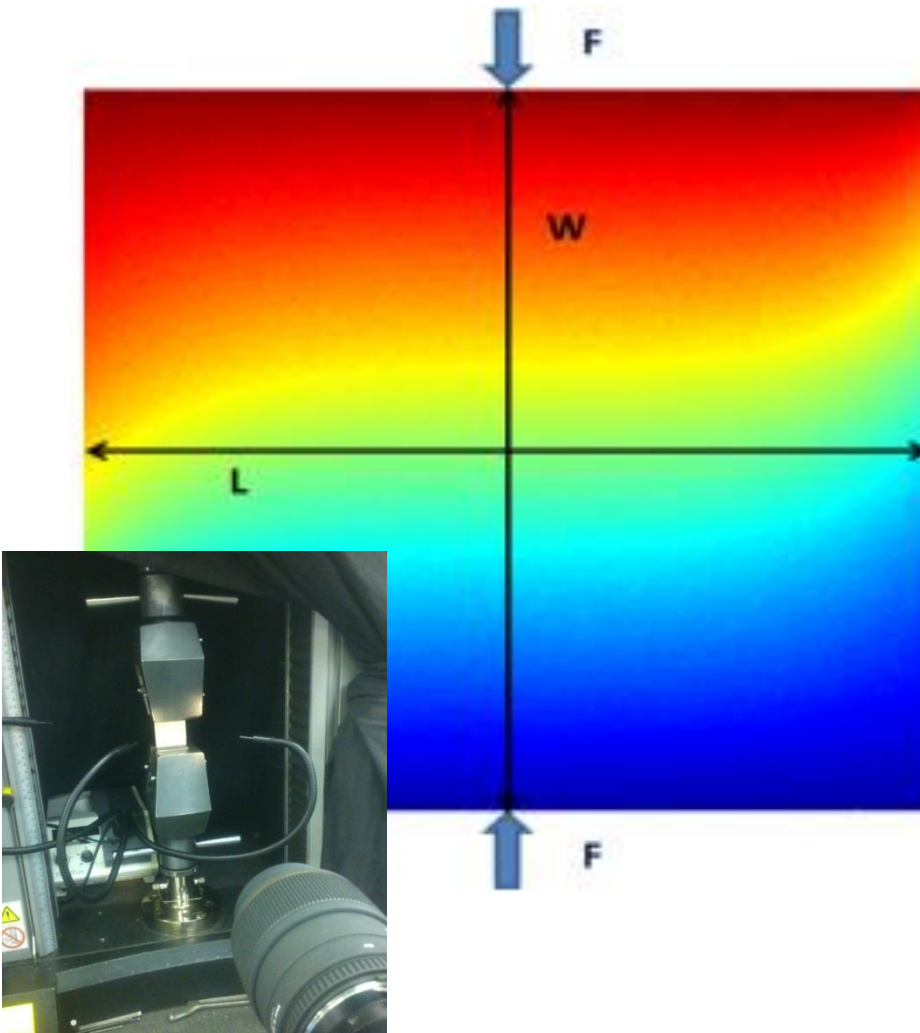


Heterogeneities ... but not too much

# Conclusions

- Simulator for material identification combining DIC and VFM
- Design specimen geometries which maximize performance of DIC and VFM
- Select the optimum regularization parameters (subset, VSG, ...) that minimize the error on the identified properties in function of your experimental setup ( noise, lighting, ...)
- Provided realistic confidence margins for the identified stiffnesses
- Applied to any material model

# Demo of direct integration of VFM and DIC



- Glass/epoxy unidirectional composite
- Linear elastic orthotropic
- Fibre orientation: 80 degrees
- Load: 3736N
- Thickness: 1mm
- Width = length = 20mm

Reference values:

$$Q_{11} = 41000\text{MPa}$$

$$Q_{22} = 10300\text{MPa}$$

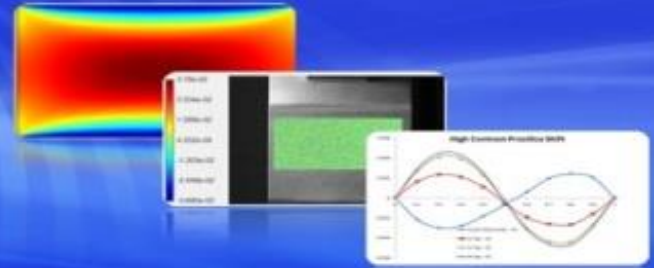
$$Q_{12} = 3090\text{MPa}$$

$$Q_{66} = 4000\text{MPa}$$

# DIC course

Metrology beyond colors

January 12-16, 2015 - Ghent, Belgium



<http://diccourse.matchid.org>

**KU LEUVEN**